Dense Granular Flow

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Wealth of Applications

technical



food processing

and in nature



random close packing Chaikin et al. 2004









ring of Saturn

... of Fundamental Interest

nonequilbrium model system

- grain of sand of diameter d at room temperature: $\frac{k_B T}{med} \sim 10^{-12}$
- interactions between macroscopic bodies are dissipative
- Grains left to themselves settle into static packing
- decay of an initially agitated state: cooling
- Dynamics due to driving, e.g. gravity, shear, fluidized beds,...

rheology of dense granular matter

How do these materials flow in response to an applied shear

Rheology of dense granular matter

How do these materials flow in response to an applied shear?



apply a stress (force/area) and measure the velocity or strain rate

$$\dot{\gamma} = \partial_y v_x$$

apply a velocity or displacement and measure the stress

Rheology of dense granular matter

What is the relation between stress and strainrate?

$$\sigma(\dot{\gamma}) = \eta(\dot{\gamma})\dot{\gamma}$$

Newtonian fluid or colloidal suspension: $\eta(\dot{\gamma}) \rightarrow \dot{\gamma}$ as $\dot{\gamma} \rightarrow 0$ fluid of athermal, hard spheres (dry granular medium):

Bagnold scaling:
$$\eta(\dot{\gamma}) \rightarrow \dot{\gamma}$$
 $\sigma \propto \dot{\gamma}^2$ as $\dot{\gamma} \rightarrow 0$

Large strainrates

shear thickening: $\eta(\dot{\gamma})$ increases with $\dot{\gamma}$ frictional granular fluid shear thinning: $\eta(\dot{\gamma})$ decreases with $\dot{\gamma}$ frictionless granular fluid



Frictionless Jamming

- ▶ jamming: a material becomes rigid with increasing packing fraction φ
- control parameters for the fluid to solid transition:
 - \blacktriangleright shear stress σ
 - \blacktriangleright packing fraction ϕ
- jamming transition is studied by monitoring flow curves





Rheology of Frictional Grains

Jamming of frictional particles



D. Bi et al., Nature 480 (2011)

phase diagram: first order phase transition and finite stress critical point in contrast to frictionless particles M. Grob, C. Heussinger and AZ, Phys. Rev. E 89, 2014

chaotic regime



Rheo-Chaos

Aradian and Cates, Phys.Rev. E73 (2005) hydrodynamic model

M. Grob, AZ and C. Heussinger, Phys.Rev. E93, (2016)

Grains with Friction

translational velocities \mathbf{v} and rotational velocities $\boldsymbol{\omega}$ Newton's equations of motion interactions only when the particles are in contact model of soft spheres: normal and tangential forces

$$F_n = -k_n \delta_n - \zeta_n v_n$$
 and $F_t = -k_t \delta_t - \zeta_t v_t$

spring constants $k_n = k_t = 1$, damping constants $\zeta_n = \zeta_t = 1$ tangential overlap: $\delta_t = \int_{t_0}^t dt' v_t(t')$ as long as $|F_t| < \mu |F_n|$

 $|F_t| = \mu |F_n| \rightarrow \text{sliding contact; no loading of the tangential spring Coulomb friction coefficient <math>\mu = 2 \rightarrow \text{strong friction}$

polydisperse mixture

strain controlled simulations (Lees Edwards boundary conditions) stress controlled simulations with rigid walls critical discussion: S. Schäfer et al., J. Phys. 16, 5, 1996



Deforming the System - Strain Controlled Simulation

impose strain rate $\dot{\gamma}$ and measure stress σ

different regimes:

- Bagnold: $\sigma \propto \dot{\gamma}^2$
- Plastic: $\sigma \propto \dot{\gamma}^{1/2}$
- φ > φ_c stress jumps, hyteresis observable
- ► still larger φ: finite yield stress

discontinuous transition; hyteresis can be observed



Proposing a Constitutive Relation - a Simple Model

• Bagnold:
$$\sigma \propto \dot{\gamma}^2 \Leftrightarrow \dot{\gamma} \propto \sigma^{1/2}$$

- Plastic:
$$\sigma \propto \dot{\gamma}^{1/2} \Leftrightarrow \dot{\gamma} \propto \sigma^2$$

• metastable: $\dot{\gamma}(\sigma)$ not monotonic

$$\dot{\gamma}(\sigma) = a\sigma^{1/2} - b\sigma + c\sigma^2$$

$$a(\phi=\phi_\eta)=$$
0; $b>0, c>0$ const.

predictions:

- discontinuous transition with a critical point
- critical point ϕ_c : vertical inflection point
- ▶ $\phi > \phi_c$: unstable region → stress jumps in the simulation
- $\phi = \phi_{\sigma} > \phi_c$: finite yield stress
- divergence of the viscosity at $\phi_{\eta} > \phi_{\sigma} > \phi_{c}$



Phase Diagram I



What happens in the unstable region? Phase separation?

Phase Coexistence?

vorticity banding

shear banding





needs third dimension and pressure has to be balenced across the interface

The Unstable Region - Stress Controlled Simulation

vary stress $\sigma_1 < \sigma_2 < \sigma_3 < \sigma_4 < \sigma_5$ at fixed ϕ monitor $\dot{\gamma}_{\sigma_i}(t)$



average over transient flow S-shaped flow curve is observed in transient behaviour



Phase Diagram II

no shear or vorticity banding shear controlled simulations unstable region: jamming metastable region: transient flow

How can we understand reentrance? reduce $\sigma \rightarrow$ reduction in normal load contacts which are blocked by the Coulomb criterion: $|F_t| < \mu |F_n|$ $|F_t| = \mu |F_n|$ become free to slide \rightarrow grains can flow \rightarrow unjamming number of sliding contacts

Florian Spreckelse





Conclusion I

- re-entrant flow
- generic feature of friction
- non-zero stress critical point
- van-der-Waals-like phenomenology

$$\dot{\gamma}(\sigma) = a\sigma^{1/2} - b\sigma + c\sigma^2$$

- 3 critical densities (Otsuki and Hayakawa, PRE 2011)
- can reproduce all features of the phase diagram
- model includes (b = 0) the frictionless case µ = 0





momentum conservation

$$\partial_t v_x = \partial_y \sigma_{xy} \to \partial_t \dot{\gamma} = \partial_y^2 \sigma$$

microstructure characterized by scalar field w(y, t);

- ► reduces strain rate as compared to the frictionless case: $\dot{\gamma} = \dot{\gamma}_0 - w$; $\dot{\gamma}_0 = a\sqrt{\sigma} + c\sigma^2$
- relaxes to a stationary value: $\partial_t w = -(w w^*)/\tau$
- stationary value $w^* = b\sigma;$ $1/ au \propto \dot{\gamma}$

Olmsted, Rheol. Acta 47, 283 (2008); Nakanishi et al., PRE 85, 011401 (2012)

Hydrodynamic Model

$$\begin{array}{rcl} \partial_t \dot{\gamma} &=& \partial_y^2 \sigma \\ \dot{\gamma} &=& \dot{\gamma}_0 - w \\ \partial_t w &=& -\dot{\gamma} (w - w^*) \end{array}$$

stationary flow: $\dot{\gamma} = a\sqrt{\sigma} - b\sigma + c\sigma^2, w = w^*, \sigma = \sigma_0$ jamming: $\dot{\gamma} = 0, w = \dot{\gamma}_0, \sigma = \sigma_0$

linear stability analysis: $\delta\sigma, \delta w \sim e^{\Omega t} e^{iky}$

stationary flow is unstable: $\frac{\partial \dot{\gamma}}{\partial \sigma} < 0$

jammed state is stable for negative $\dot{\gamma}$



Phase diagram III

predictions of the hydrodynamic model





N=24000

 $\sigma = 6.3 \times 10^{-5}$

σ=6.3×10⁻⁶

σ=1.6×10⁻⁶

Simulations:



How to characterize heterogeneous, chaotic states?

anisotropic and long ranged stress fluctuations in dilation direction length scale \sim system size



spectrum of strainrate fluctuations in stress controlled simulations



 $4\times 10^{-7} \le \sigma \le 2, 5\times 10^{-2}$

Conclusions II

- re-entrant flow, nonzero stress critical point
- van der Waals like phenomenology
- spatio-temporal chaos besides stationary flow and jamming
- observable only for sufficiently large system size
- complex frequency dependent spectra and spatial correlations on scales of system size
- Hydrodynamic model: coupled dynamics of stress and microstructure
- stability analysis: time dependent states
- microstructure $\rightarrow \dot{\gamma}(\sigma) = a\sigma^{1/2} b\sigma + c\sigma^2$





Microscopic picture of friction induced shear thickening

Shear Thickening: Ubiquitous Phenomenon

shear thickening observed in colloidal and non-Brownian suspensions



possible mechanisms:

- formation of hydroclusters
- shear induced glass transition
- viscosity of frictional system diverges at lower φ; friction becomes effective for f > f*; sharp crossover for σ > σ*
- ► enforced flow → dilation; constant volume → large normal stresses → large shear resistance

E. Brown and H. Jäger, Rep. Prog. Phys. 77, 2012; R. Seto et al. PRL 111, 2013; C. Heussinger PRE 88, 2013;
 N. Fernandez et al. PRL 111, 2013; Z. Pan et al. PRE 92, 2014; E. DeGulie et al. arXiv:1509.03512

Microscopic picture of friction induced shear thickening

Frictionless granular media shear thin Frictional granular media shear thicken

dense suspensions: frictional contact forces and viscous drag



Growing length scale in shear thickening regime

C. Heussinger PRE 2013



FIG. 4. Velocity correlation function $C_v(x) = \langle v_y(x)v_y(0) \rangle$ for different strain rates and $\phi = 0.7935$.

2 particles in contact:

frictional forces reduce relative motion at the contact point:

$$g=v_1^t-v_2^t+rac{1}{2}(d_1\omega_1+d_2\omega_2)
ightarrow 0$$

2 extreme cases:

rotations adapt without generating relative translational motion

exchange of translational and rotational velocities such that

$$v_1^t \sim v_2^t; \quad d_1 \omega_1 \sim -d_2 \omega_2$$

 $\mathbf{v}\sim\mathbf{d}\omega$

extend 2-particle picture to patch of size $\boldsymbol{\xi}$

ball bearing state with no relative slip and weak shear resistance



Aström et al. PRL **84**, 638 (2000) Alonso-Marroquin et al. PRE **74**, 031306 (2006) Tordesillas et al. PRE **81**, 011302 (2010) PRE **86**, 011306 (2012) packing with highest density: all particles in frustrated loops







clockwise: red anti-clockwise: blue

mosaique structure: solid like patches coexisting with clusters of strongly rotating particles



lines: nonaffine velocities; only large ω are shown

see also Henkes et al. \rightarrow rigidity percolation



strongly increasing number of 3-loops in the ST regime; solidlike vortices

Conclusions III

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- ► Hydrodynamic model: coupled dynamics of stress and microstructure
- stability analysis: time dependent states
- microstructure $\rightarrow \dot{\gamma}(\sigma) = a\sigma^{1/2} b\sigma + c\sigma^2$
- microscopic picture: mosaique structure of solid like (frustrated) patches and clusters of strongly rotating particles







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